

## Full Power Operation of a Synchrotron Magnet Power Supply in Dual Resonant Frequency Mode

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### ABSTRACT

A synchrotron magnet power supply aimed at practical use was constructed and successfully operated in dual resonant frequency mode. A magnet exciting current was 1300A, and values of resonant frequency were 100/3Hz for acceleration period and 100Hz for magnet reset period, respectively, resulting in an average frequency of 50Hz.

### INTRODUCTION

A dual resonant frequency circuit for a synchrotron magnet system was first proposed by M. Foss and W. Praeg.<sup>[1]</sup> In their circuit two frequencies were alternated each other by switching a part of the resonant capacitor with an inverter type thyristor. This operation utilizes most of accelerator cycle for beam acceleration and consequently reduces the RF accelerating voltage which is required in single frequency operation.

Our circuit is the similar one but the thyristor is replaced by a gate-turn-off thyristor (GTO). Alternative frequencies were chosen 100/3Hz for acceleration period and 100Hz for magnet reset period, respectively, so that average frequency of 50Hz was obtained. The behavior of the circuit has been studied with a model circuit,<sup>[2]</sup> and feasibility of this circuit was confirmed. Taking account of the results, we constructed the magnetic power supply aimed at practical use. In the present paper, we describe its performance.

### CIRCUIT DESCRIPTION

The resonant system is illustrated in Fig. 1, and parameters of the circuit are listed in Table 1. This circuit consists of two parts; the dual resonant frequency circuit and a pulse power supply. The pulse power supply feeds the power consumed in the resonant circuit with a pulse current at each acceleration period. The basic performance of the resonant circuit was described elsewhere<sup>[2]</sup>. For the present circuit, in order to protect the GTO against large forward voltage drop, we replaced the diode, which was used in the model circuit, by a thyristor denoted by SCR<sub>g</sub> in the figure. The switching timing of the SCR<sub>g</sub> is made to coincide with the GTO.

A snubber circuit is composed of a diode D<sub>s</sub>, capacitor C<sub>s</sub> and resistor R<sub>s</sub>. When the GTO is turned off, C<sub>s</sub> begins to absorb the GTO current through D<sub>s</sub>. After the capacitor voltage reaches maximum, the capacitor C<sub>s</sub> discharges through R<sub>s</sub>. This action suppress the rapid rise of the voltage across the GTO and ensures its safety operation.

Fig. 2 shows waveforms of the magnet voltage, magnet current I<sub>m</sub> and the GTO current I<sub>g</sub> when the system was operated with maximum rating. Here, amplitudes of the magnet voltage and current were 2800V (at 100Hz) and 1300A, respectively. The maximum current through the GTO was observed to be 1200A. Current waveforms of the GTO, the resonant capacitor C<sub>1</sub> and the magnet for one accelerator period are shown in Fig. 3. A damping oscillation of 2.5kHz is observed in the capacitor current

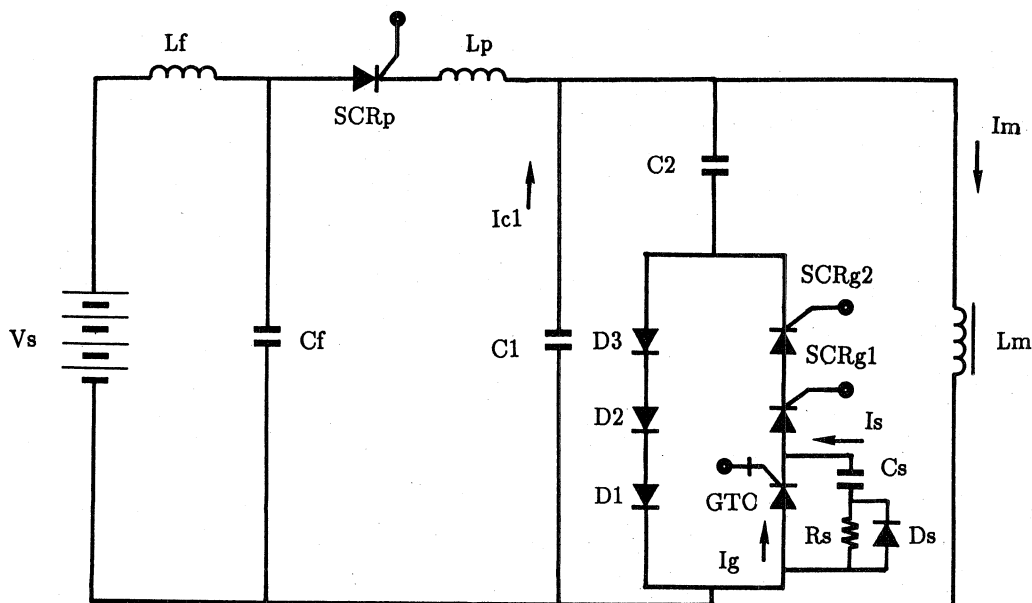


Fig. 1 Diagram of the resonant system

$I_{C1}$  at the beginning of the acceleration period. This phenomenon is caused by an alternative current between capacitors C1 and C2. The effect due to this oscillating current was observed like a dip on the waveform of the magnetic field, as shown in Fig. 4. This disturbance amounted to 0.4% of the amplitude of the magnetic field.

Table 1

Parameters of Dual Resonant Circuit

- Pulse power supply -

|                       |                       |
|-----------------------|-----------------------|
| DC power supply $V_s$ | 1100V                 |
| Capacitor $C_f$       | Capacity 93.4 $\mu$ F |
|                       | Peak voltage 2200V    |
| Inductor $L_f$        | Inductance 1.73H      |
| Inductor $L_p$        | Inductance 12mH       |
| Thyristor SCRp        | CR100AL-24(HITACHI)   |
|                       | 100A/1200V            |

- Dual frequency system -

|                |                                     |
|----------------|-------------------------------------|
| Capacitor C1   | Capacity 859 $\mu$ F                |
|                | peak voltage 3300V                  |
|                | peak current 1800A                  |
| Capacitor C2   | Capacity 6870 $\mu$ F               |
|                | peak voltage 1100V                  |
|                | peak current 1600A                  |
| Magnet $L_m$   | Inductance 2.9mH                    |
|                | peak voltage 3300V                  |
|                | peak current 1800A                  |
| Diode D1 to D3 | C01DA(HITACHI)                      |
|                | 800A/3000V                          |
| Thyristor SCRg | CA01CF(HITACHI)                     |
|                | 1000A/2500V                         |
| GTO thyristor  | GFP2000B25(HITACHI)                 |
|                | peak off-state voltage 2500V        |
|                | rms-on-state current 800A           |
|                | Controllable on-state current       |
|                | in repetitive case 2000A            |
|                | peak on-state voltage 2.5V at 2000A |

- Snubber circuit -

|                 |                                |
|-----------------|--------------------------------|
| Capacitor $C_s$ | Capacity 6 $\mu$ F             |
| Resistor $R_s$  | Resistance 2.3 $\Omega$ (800W) |
| Diode $D_s$     | DFS80B17                       |
|                 | 80A/1700V                      |

At the end of the acceleration period, sharp disturbance on the magnetic field is seen as shown in Fig. 5. This disturbance was also observed in the voltage and current waveforms of the magnet at the same time. Therefore, there may be some origin although it is not confirmed. Such a deformation of the waveform was estimated to be 2.7% of the amplitude. Fig. 6 shows the waveforms of the snubber current  $I_s$  and the GTO current  $I_g$  when the GTO turns off. While the GTO current turns off within 2 $\mu$ sec, the snubber current decreases more slowly. Total amount of the turn-off time of the current of the branch containing the GTO was about 20 $\mu$ sec. It is, however, sufficiently enough for our circuit, since the average repetition rate is 50Hz.

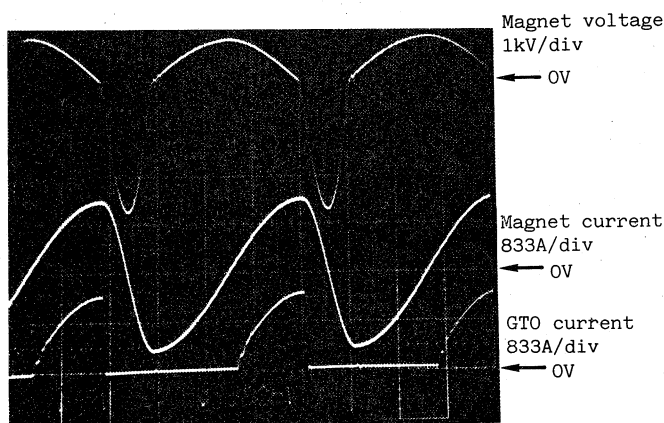


Fig. 2 Voltage and current waveforms of the magnet and GTO current

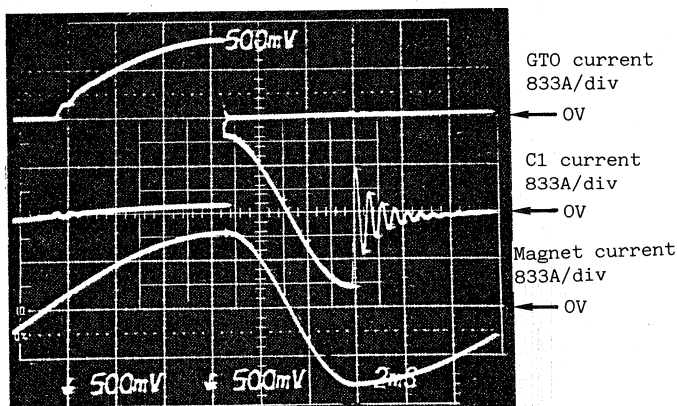


Fig. 3 Current waveforms of GTO, C1 and Magnet

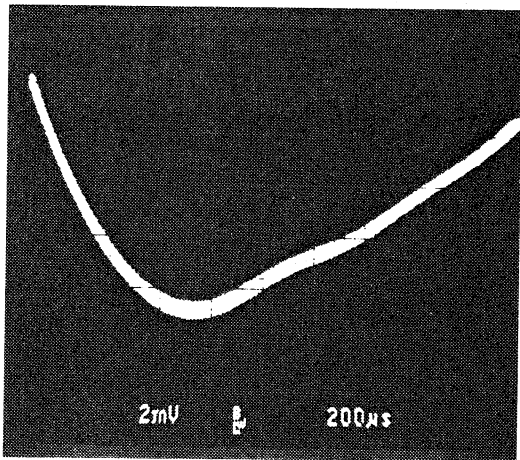


Fig. 4 Waveform of the magnetic field around the beginning of the acceleration period

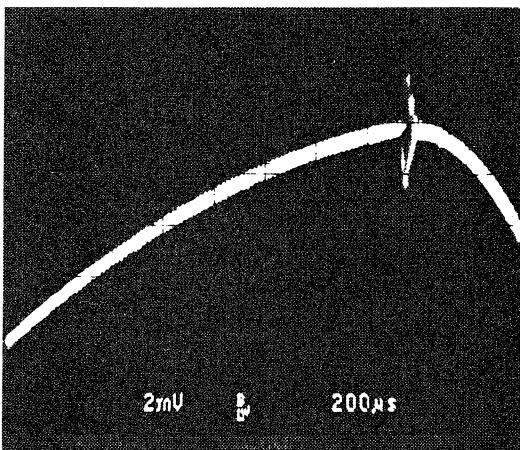


Fig. 5 Waveform of the magnetic field around the end of the acceleration period

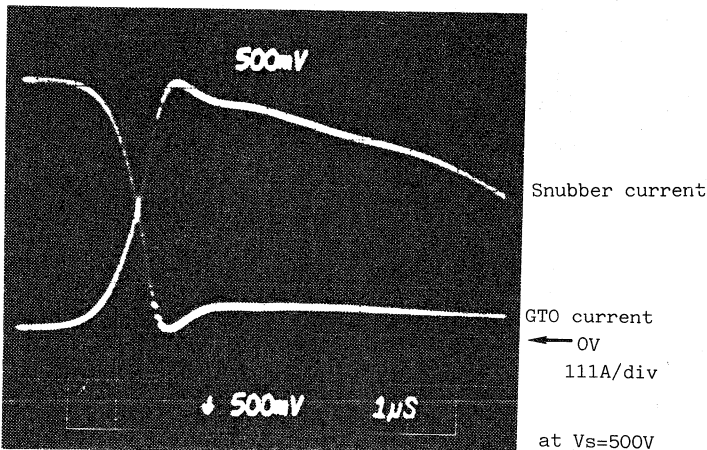


Fig. 6 Current waveform of GTO and snubber circuit

## SUMMARY

An operation of the dual resonant frequency circuit aimed at practical use was performed successfully. The magnetic field suffers some disturbances at extremes of the acceleration period. At the beginning of the acceleration period, fortunately, it is negligible practically with respect to the amplitude of the magnetic field. However, some consideration may be needed to avoid an error field at the end of the acceleration period. In order to achieve the excitation of the synchrotron magnet, a dc-magnetic field is needed. Therefore, we are preparing a dc-power supply and a choke transformer which is used for superposition of ac and dc-current.

## ACKNOWLEDGEMENTS

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## REFERENCES

1. M. Foss and W. Praeg, IEEE, Trans. Nucl. Sci., NS-28, 2856 (1981)
2. H. Someya et. al., IEEE, Trans. Nucl. Sci., NS-32, 3775 (1985)